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Cryogenic Impinging Jets Subjected to High Frequency Transverse Acoustic Forcing in a High Pressure Environment

24-27 July 2016
Joint Propulsion Conference



Mario Roa, Sierra Lobo, Inc. Alex Schumaker, AFRL Doug Talley, AFRL



Objectives



- Study impinging jets, with N2 as the working fluid, under sub and supercritical conditions.
- Vary jet velocity and chamber pressure to identify conditions where impact waves became prominent, for a single geometry.
- Study the flow field with high speed back light imaging.
 Perform dynamic mode decomposition (DMD) analysis to extract natural frequencies.
- Study the response of the flow field when driven by acoustic speakers at low amplitude, high frequency standing wave in pressure anti-node and pressure node configuration.



Impinging Jet Injector



Features

- An injector design where fluid jets strike each other.
- An impingement sheet is formed and impact waves, or surface waves, develop on the surface
- The impinging jet injectors are used to atomize storable liquid rocket engine fuels. They are desirable because of their:
 - Simplicity
 - Low manufacturing cost
 - Good atomization and mixing
- Highly susceptible to instabilities

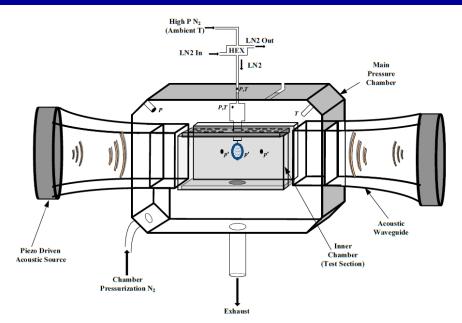


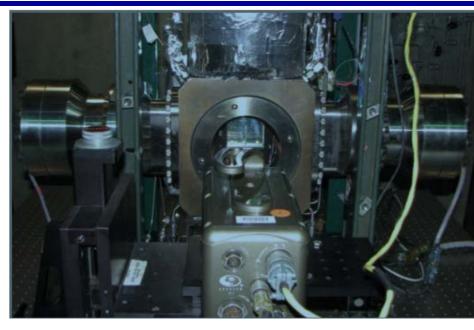
Chihiro Inoue Department of Aeronautics and Astronautics University of Tokyo



Experimental Facility







Features

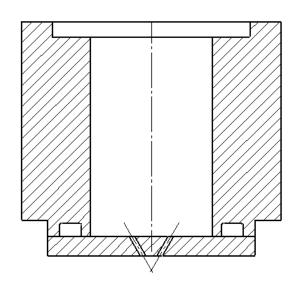
- Two piezosirens designed for high pressure operation.
- Accurate control of frequency and amplitude of the standing wave. Within \pm 0.1 Hz frequency.
- Multiple high-speed pressure transducers
- A low flow pressurization accurate control of pressure.
 - Subcritical and supercritical pressures
- Heat changers to create liquid nitrogen accurate control of temperature to within ±5 K.
- On-axis windows for shadowgraph and Schlieren.



Operating Conditions



- Vary chamber pressure until impact waves, or surface waves, became prominent on the impingement sheet.
 - Jet velocities from 0.5 to 15 m/s
 - Chamber pressures of 0 to 4.8 MPa
- The conditions where impact waves were prominent were for jet velocities of 2 to 5 m/s and chamber pressures of 1 to 1.37 MPa (150 to 200 Psi).
 - 2 m/s and Chamber pressure of 1.37 MPa was selected for further study (Re # = 7800 and We # = 270).
- High speed back-light images were captured at 25kHz.
- N2 jet temperature was kept at a constant 95 K.
- Orifice diameter 0.5 mm (0.02in), pre-impingement length 8 I/D and 5 I/D channel length.
- Impingement half angle is 30 degrees.

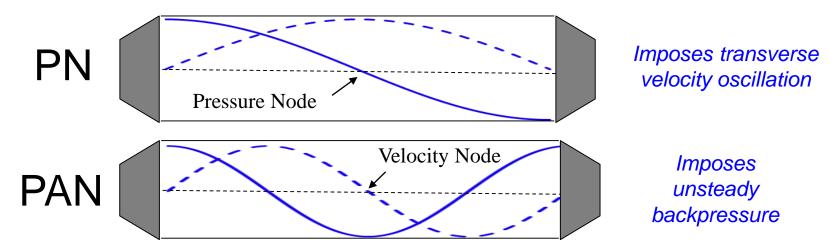




Forcing Conditions



Pressure node (PN) and pressure antinode (PAN) at the injector location



- Forcing frequency ~ 3000 Hz
- Pressure fluctuation amplitudes (peak-to-peak) range up to approximately 9 psi (2% of Chamber Pressure)

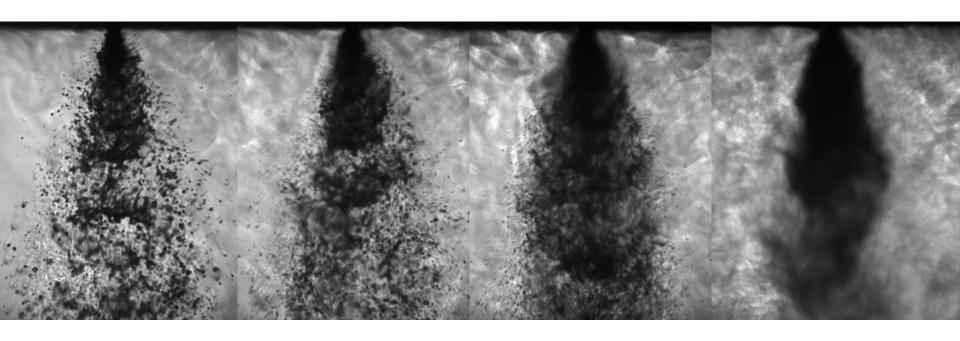


Parametric Sweep Sub-Critical Results



1.72 MPa (250 Psi)

5 m/s 7 m/s 10 m/s 20 m/s



- A droplet size decreases as jet velocity increases
- There are no noticeable structures on the impingement sheet.

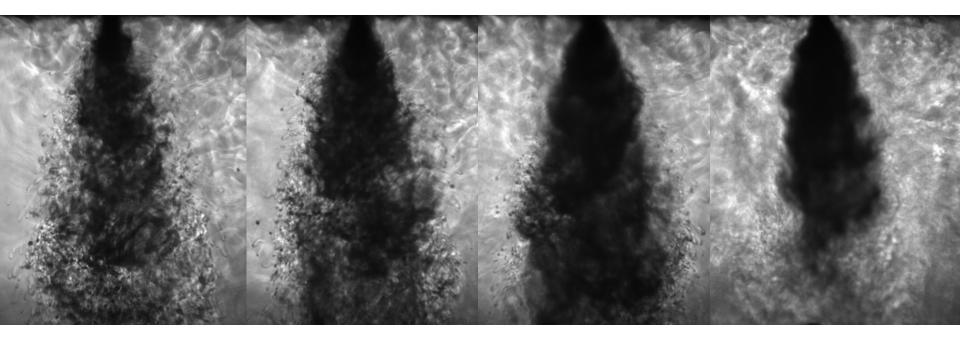


Parametric Sweep Sub-Critical Results



2.58 MPa (375 Psi)

5 m/s 7 m/s 10 m/s 20 m/s



 Transition to a fine mist occurs at lower velocities at high pressures.



Parametric Sweep Super-Critical Results



4.82 MPa (700 Psi)

5 m/s 7 m/s 10 m/s

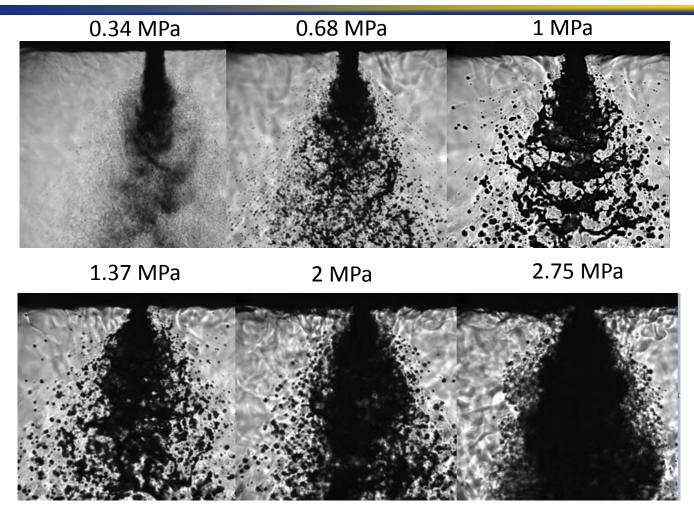
Differences between subcritical:

- The interface between the surrounding the impingement sheet seem blurred.
- No structure were noticed on the impingement sheet.



Parametric Sweep 2 m/s Results





- The jet velocity was kept at a constant 2 m/s
- The chamber pressure was increased close to supercritical pressure.
- Impact waves appeared for a narrow range of operating conditions.



Dynamic Mode Decomposition



Extract spectrally-pure temporal modes with detailed spatial mode shapes

- Schmid (2010) and Rowley et al. (2009)
- Employ time-averaged amplitude measurement described by Alenius (2014)
 Amplitude of mode at t = 0
- 1500 samples used

$$I(x, y, t) = \operatorname{Re}\left(\sum_{i=1}^{n} \widetilde{A}_{i} \exp(\widetilde{\lambda}_{i} t) \widetilde{D}_{i}(x, y)\right)$$
average image
Accounts for growth of

Time average image subtracted from data

Accounts for growth of mode in time as well as temporal frequency

Complex spatial mode shape

Properties of DMD

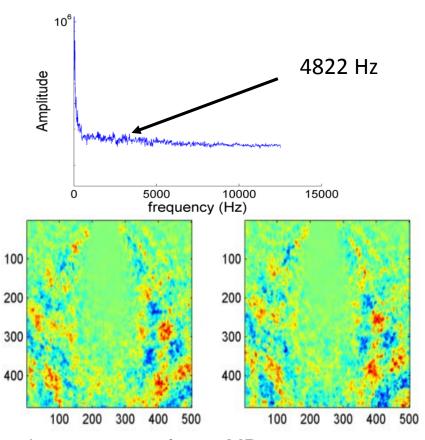
- Isolates response of flow at forcing frequency and harmonics
- Single modes can reconstruct convective processes (POD requires two modes)
- Less efficient at reconstructing signal energy compared to POD



DMD Result, Unforced







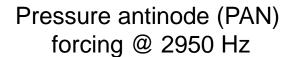
- The jet was kept at a constant 2 m/s at chamber pressure of 1.37 MPa.
- DMD was applied only on the impingement sheet.
- Impact waves were not a dominant feature of the flow field based on the DMD analysis.
- There is a large amount of variability as to when the impact wave detaches and convective velocity.

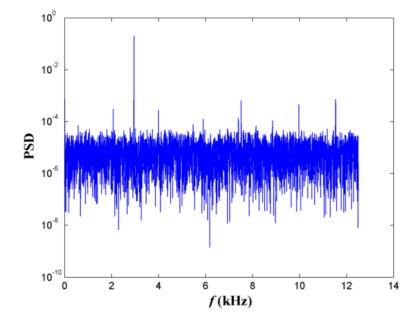


PSIA

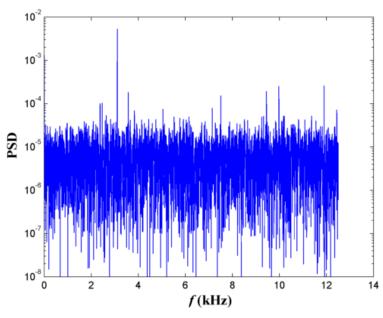
PAN Acoustic Forcing







Pressure node (PN) forcing @ 3110



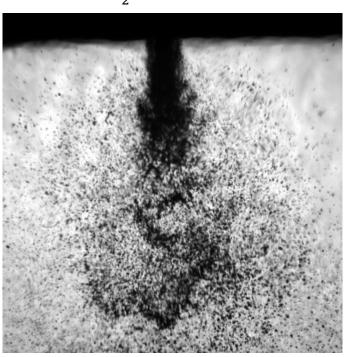


Acoustic Forcing: Max



PAN Forcing

$$\frac{P'}{\frac{1}{2}\rho u^2} = 58.1$$



PN Forcing

$$\frac{P'}{\frac{1}{2}\rho u^2} = 40$$

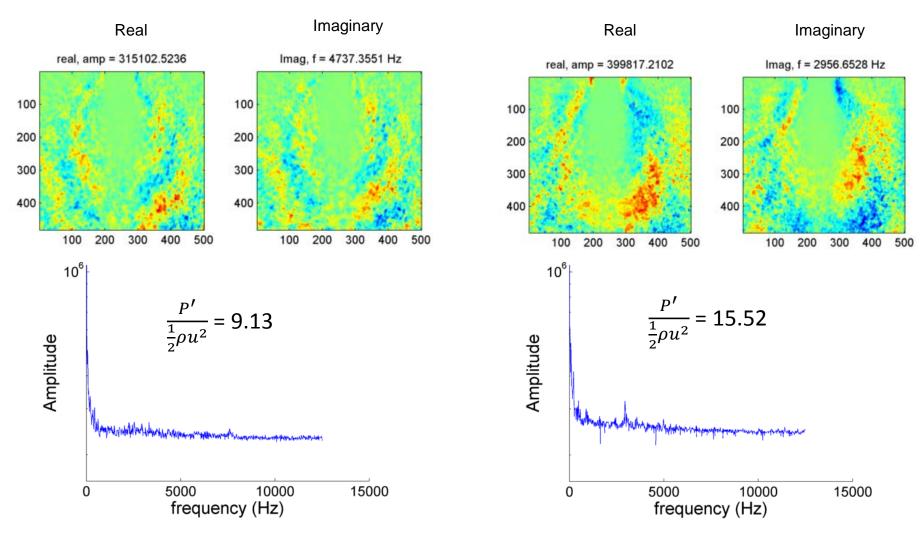


 Impact waves appear to vanish at a critical pressure forcing amplitude. The forcing amplitude is different for PAN and PN forcing.



Forcing PAN: Results



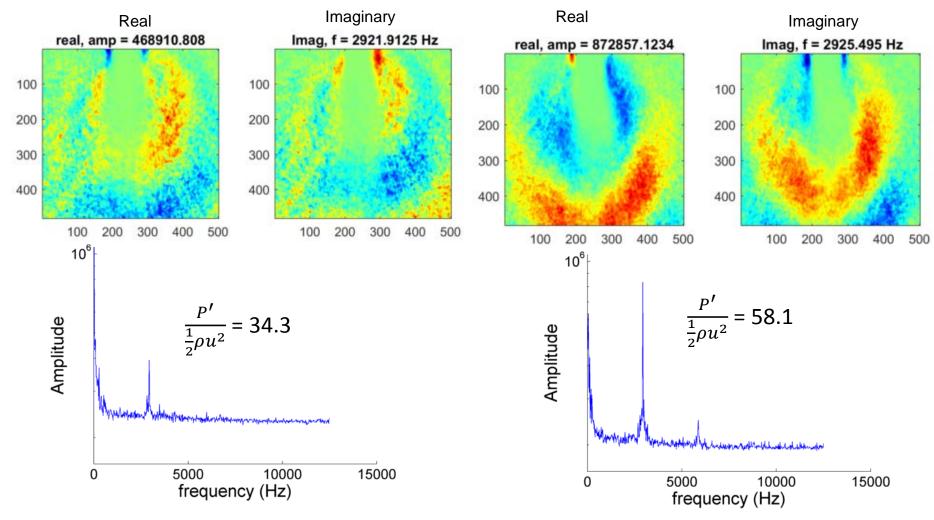


Impact waves are still present at low level PAN forcing.



Forcing PAN: Results



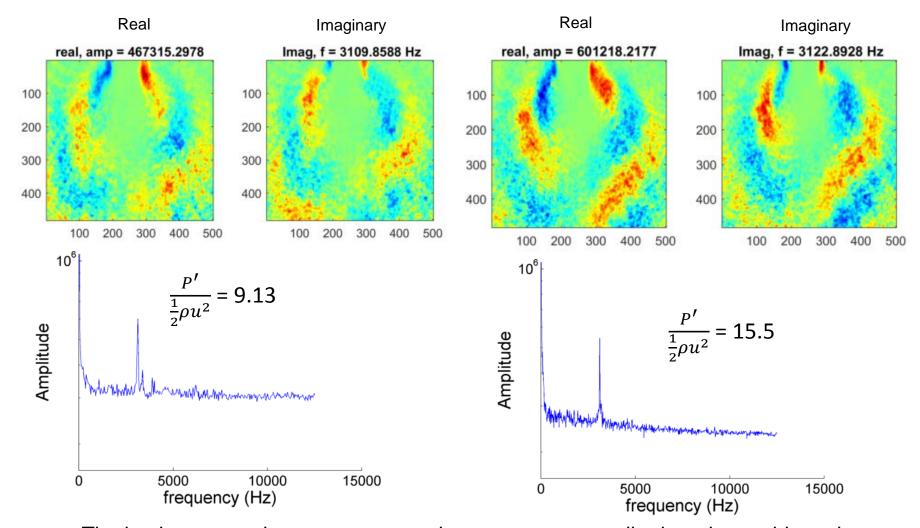


- Impact waves structures have vanished from the impingement sheet.
- Cyclical mass flow variations dominant the flow field.



Forcing PN: Results



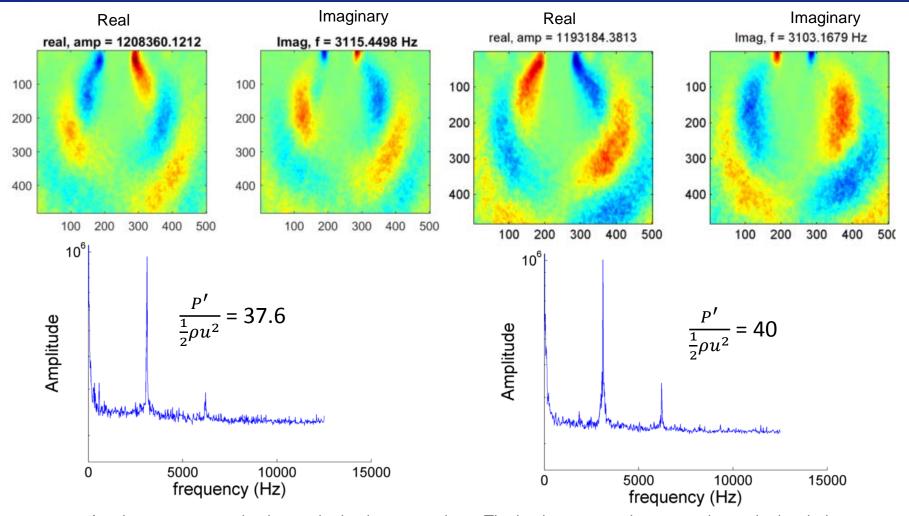


 The impingement sheet responses at lower pressure amplitudes when subjected to PN forcing.



Forcing PAN: Results





- A swig-swag pattern dominants the impingement sheet. The impingement point moves due to the jets being displaced.
- Impact waves also vanished at a critical pressure amplitude and ligaments are shed due to acoustic forcing.

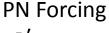


Phased Average: Max Forcing

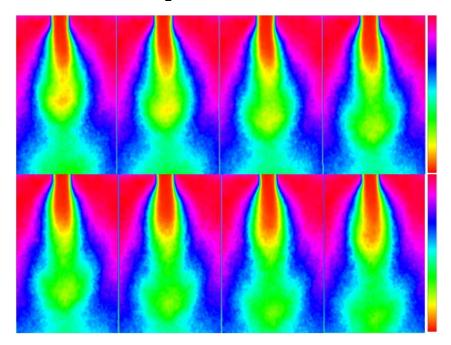


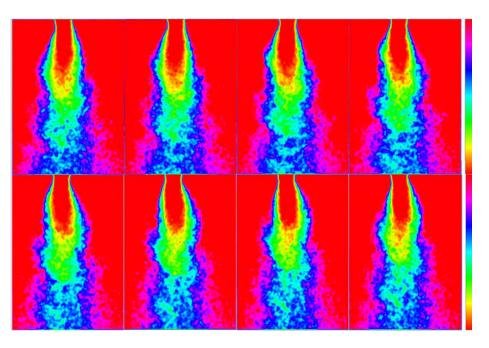
PAN Forcing

$$\frac{P'}{\frac{1}{2}\rho u^2} = 58.1$$



$$\frac{P'}{\frac{1}{2}\rho u^2} = 40$$





- For the PAN forcing, a large group of droplets are shed at the acoustic forcing frequency due to mass flow variations.
- A swig-swag pattern is present when the impingement sheet is subjected to PN forcing.



Conclusions, unforced



- Impact waves, or surface waves, appeared in a narrow range of operating conditions for the given injector.
- Dynamic mode decomposition was unable to detect a strong natural frequency associated with impact waves.
- For supercritical conditions the injection process and the emerging fluid has to be modelled differently compared to sub-critical conditions
- There is large amount of variability from the flow field (convective velocity or ligament separation) to detect a single, strong natural frequency associated with impact wave conditions



Conclusions, forced



- The impingement sheet couples with the acoustics at a certain level of acoustic amplitude
 - The critical pressure amplitude is different for PAN and PN forcing.
- Dynamic mode decomposition detected the onset of the coupling and higher harmonics when the forcing was greater than the critical pressure amplitude
- PAN forcing:
 - Mass flow variations
 - Due to the klystron effect results in a "Christmas tree" look.
- PN Forcing
 - Results in a swig-swag pattern on the impingement sheet
 - Probably due to a impingement point physically moving



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